

## **CERTIFICATION REPORT**

**The certification of the absorbed energy (150 J nominal) of Charpy V-notch reference test pieces for tests at 20 °C**

**Certified Reference Material ERM ®-FA415z**

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Joint Research Centre  
Institute for Reference Materials and Measurements

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**Certified Reference Material ERM ®-FA415z**

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## Summary

This certification report describes the processing and characterisation of ERM®-FA415z, a batch of Charpy V-notch reference test pieces certified for the absorbed energy (*KV*) for tests at 20 °C. Sets of five of these test pieces are used for the verification of pendulum impact test machines according to ISO 148-2 (Metallic materials - Charpy pendulum impact test – Part 2: Verification of testing machines [1]).

The measurand *KV* is procedurally defined and refers to the impact energy required to break a V-notch test piece of standardised dimensions, as defined in ISO 148-1 [2]. The certified value of ERM- FA415z is traceable to the SI, via the SI-traceable certified value of the master batch ERM-FA415s, by testing samples of ERM-FA415z and ERM-FA415s under repeatability conditions on an impact pendulum verified and calibrated with SI-traceable calibrated tools. The certified value is valid only for strikers with a 2 mm tip radius. The certified values are valid at  $(20 \pm 2)$  °C.

The certified values for *KV* (= energy required to break a V-notch test piece using a Charpy pendulum impact test machine) and the associated expanded uncertainties ( $k = 2$ , corresponding to a confidence level of about 95 %) calculated for the mean of a set of five test pieces, are:

Steel Charpy V-notch test pieces		
	Certified value <sup>2)</sup> [J]	Uncertainty <sup>3)</sup> [J]
Absorbed energy ( <i>KV</i> ) at 20 °C <sup>1)</sup>	153	5
<p>1) The absorbed energy (<i>KV</i>) is a method defined measurand. <i>KV</i> is the impact energy required to break a V-notched bar of standardised dimensions, as defined in ISO 148-1. The certified value is valid only for strikers with a 2 mm tip radius, and in the temperature range of <math>(20 \pm 2)</math> °C.</p> <p>2) The certified value of ERM-FA415z, and the associated uncertainty, are traceable to the International System of Units (SI), via the master batch ERM-FA415s, of the same nominal absorbed energy (150 J) by testing samples of ERM-FA415z and ERM-FA415s under repeatability conditions on an impact pendulum verified and calibrated with SI-traceably calibrated tools.</p> <p>3) Estimated expanded uncertainty of the mean <i>KV</i> of the five specimens (delivered as one set), with a coverage factor <math>k = 2</math>, corresponding to a level of confidence of about 95 %, as defined in ISO/IEC Guide 98-3, Uncertainty of measurement – Part 3: Guide to the expression of uncertainty in measurement (GUM:1995). The number of degrees of freedom of the certified uncertainty is <math>\nu_{RM} = 35</math>.</p>		



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## Glossary

AISI	American Iron and Steel Institute
ASTM	American Society for Testing and Materials
BCR	Community Bureau of Reference
CRM	Certified Reference Material
EC	European Commission
ERM <sup>®</sup>	European Reference Material
IMB	International Master Batch
IRMM	Institute for Reference Materials and Measurements
ISO	International Organization for Standardization
JRC	Joint Research Centre
$k$	Coverage factor
$KV$	Absorbed energy = energy required to break a V-notched test piece of defined shape and dimensions using a pendulum impact testing machine
$KV_{CRM}$	Certified $KV$ value of a set of 5 reference test pieces from the Secondary Batch
$KV_{MB}$	Certified $KV$ value of the Master Batch test pieces
LNE	Laboratoire national de métrologie et d'essais
MB	Master Batch
$n_{MB}$	Number of samples of the Master Batch tested during certification of the Secondary Batch
$n_{SB}$	Number of samples of the Secondary Batch tested for certification
$RSD$	Relative standard deviation
$s$	Standard deviation
SB	Secondary Batch
$s_h$	Standard deviation of the results of the samples tested to assess the homogeneity of the Secondary Batch
$s_{MB}$	Standard deviation of the $n_{MB}$ results of the samples of the

	Master Batch tested for the certification of the Secondary Batch
$s_{SB}$	Standard deviation of the $n_{SB}$ results of the samples tested for the characterisation of the Secondary Batch
$u_{CRM}$	Combined standard uncertainty of $KV_{CRM}$
$U_{CRM}$	Expanded uncertainty ( $k = 2$ , confidence level of about 95 %) of $KV_{CRM}$
$u_{char}$	Standard uncertainty of the result of the characterisation tests
$u_{char,rel}$	Relative standard uncertainty of the result of the characterisation tests
$u_h$	Contribution to uncertainty from homogeneity
$u_i$	Value of uncertainty from contribution i
$u_{MB}$	Standard uncertainty of $KV_{MB}$
$u_{MB,rel}$	Relative standard uncertainty of $KV_{MB}$
% m/m	Mass fraction
$\bar{X}_{MB}$	Mean $KV$ value of the $n_{MB}$ measurements on samples of the Master Batch tested when characterising the Secondary Batch
$\bar{X}_{SB}$	Mean $KV$ value of the $n_{SB}$ results of the samples tested for the characterisation of the Secondary Batch
$\Delta h$	difference between the height of the centre of gravity of the pendulum prior to release and at the end of the half-swing during which the sample is broken
$\nu_{RM}$	Effective number of degrees of freedom associated with the uncertainty of the certified value

# 1 Introduction

## 1.1 The Charpy pendulum impact test

The Charpy pendulum impact test is designed to assess the resistance of a material to shock loading. The test, which consists of breaking a notched bar of the test material using a hammer rotating around a fixed horizontal axis, is schematically presented in Figure 1.

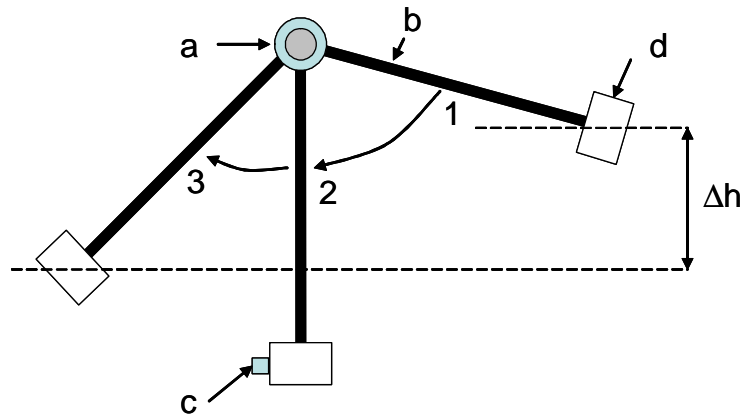


Figure 1: Schematic presentation of the Charpy pendulum impact test, showing a: the horizontal rotation axis of the pendulum, b: the stiff shaft on to which is fixed d: the hammer. The hammer is released from a well-defined height (position 1). When the hammer has reached maximum kinetic energy (shaft in vertical position 2), the hammer strikes c: the test sample, which is positioned on a support and against the pendulum anvils (not shown). The height reached by the hammer after having broken the sample (position 3) is recorded. The difference in height between position 1 and 3 ( $\Delta h$ ) corresponds with a difference in potential energy, and is a measure of the energy required to break the test sample.

The energy absorbed by the test sample is very dependent on the impact pendulum construction and its dynamic behaviour. Methods to verify the performance of an impact pendulum require the use of reference test pieces as described in ISO and other international standards [1, 3]. The reference test pieces dealt with in this report comply with a V-notched test piece shape of well-defined geometry [1], schematically shown in Figure 2.

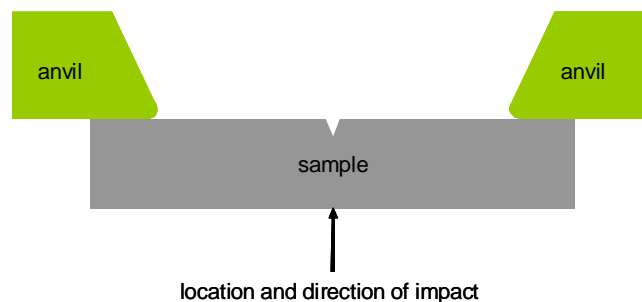


Figure 2: Schematic drawing of a V-notched Charpy test piece (top-view), indicating the place and direction of impact.

## **1.2 The certification concept of Master Batch and Secondary Batch**

### **1.2.1 Difference between Master and Secondary Batches**

The BCR reports by Marchandise et al. [4] and Varma [5] provide details of the certification of BCR “Master Batches” (MB) of Charpy V-notch certified reference test pieces. The certified value of a Master Batch is obtained using an international laboratory intercomparison.

This report describes the production of a “Secondary Batch” (SB) of Charpy V-notch certified reference test pieces at the Institute for Reference Materials and Measurements (IRMM) of the European Commission's (EC) Joint Research Centre (JRC). The work was performed in accordance with procedures described in the BCR reports [4] and [5]. The certification of a SB is based on the comparison of a set of SB test pieces with a set of test pieces from the corresponding MB under repeatability conditions on a single pendulum.

The BCR reports [4] and [5] were published in 1991 and 1999, respectively. Since 2000, the calculation of the certified value and the estimation of its uncertainty have been updated to an approach compliant with the ISO/IEC Guide to the Expression of Uncertainty in Measurement [6]. This revised approach was developed and presented by Ingelbrecht et al. [7, 8], and is summarised below.

### **1.2.2 Certification of a Secondary Batch of Charpy V-notch test pieces**

The certified absorbed energy of a SB of Charpy V-notch reference test pieces ( $KV_{CRM}$ ) is calculated from the mean  $KV$ -value of a set of SB-samples ( $\bar{X}_{SB}$ ) tested on a single pendulum. This value  $\bar{X}_{SB}$  has to be corrected for the bias of this particular pendulum. The bias of the pendulum at the moment of testing the samples of the SB, is estimated by comparing the mean  $KV$ -value of a number of samples of the MB ( $\bar{X}_{MB}$ ), tested together with the SB samples under repeatability conditions, with the certified value of the MB ( $KV_{MB}$ ).  $KV_{CRM}$  is then calculated as follows [8]:

$$KV_{CRM} = \left[ \frac{KV_{MB}}{\bar{X}_{MB}} \cdot \bar{X}_{SB} \right] \quad \text{Eq. 1}$$

For this approach to be reliable, the pendulum used for the tests on MB and SB in repeatability conditions, must be well performing. In other words, the ratio  $\frac{KV_{MB}}{\bar{X}_{MB}}$  must be close to 1. IRMM allows a difference of 5 % ( $KV_{MB} \geq 40$  J) or 2 J ( $KV_{MB} < 40$  J) between  $KV_{MB}$  and  $\bar{X}_{MB}$ , corresponding with the level of bias allowed for reference pendulums specified in ISO 148-3 [9].

Also, for reasons of commutability, a comparable response of the pendulum to the MB and SB samples is required. This is the reason why MB and SB samples are made from nominally the same steel. Moreover, it is checked that

the ratio  $\frac{KV_{CRM}}{KV_{MB}}$  is close to 1. IRMM allows a difference of 20 % ( $KV_{MB} \geq 40$  J) or 8 J ( $KV_{MB} < 40$  J) between  $KV_{CRM}$  and  $KV_{MB}$  to ensure that the MB and SB samples have a comparable interaction with the pendulum.

### 1.2.3 Uncertainty of the certified value of a Secondary Batch of Charpy V-notch test pieces

The uncertainty of the certified value of the SB is a combination of the uncertainties of the right-hand side factors in Eq. 1. It is clear that the MB-SB approach necessarily results in a larger uncertainty of the certified value of SB in comparison with the MB. The additional uncertainty depends on the uncertainty of the ratio  $\bar{X}_{SB}/\bar{X}_{MB}$ . The full measurement uncertainty of the values  $\bar{X}_{MB}$  and  $\bar{X}_{SB}$  is relatively large. However, when all conditions mentioned above (repeatability conditions, pendulum performance, and commutability between Secondary and Master Batch) are fulfilled, then the uncertainties of the values  $\bar{X}_{MB}$  and  $\bar{X}_{SB}$  have several contributions in common, in particular the uncertainty due to the bias of the pendulum. These shared uncertainty components do not contribute to the uncertainty of the ratio  $\bar{X}_{SB}/\bar{X}_{MB}$ , and only the standard deviations of the SB and MB results in the MB-SB comparison test need to be taken into account (see also Section 6.3). Thus, the MB-SB comparison approach can produce a value for the uncertainty of  $KV_{CRM}$  that is sufficiently small to meet the requirements of the intended use of the certified reference material (CRM).

## 2 Participants

The processing of the SB (ERM-FA415z) test pieces was carried out by the Institut für Eignungsprüfung GmbH (IfEP), Marl (DE), using steel bars produced at Aubert&Duval, Les Ancizes (FR).

The MB samples (ERM-FA415s) used in the characterisation of the SB were provided by IRMM, Geel (BE).

The homogeneity of the SB was evaluated based on data obtained at IfEP using a pendulum verified according to the criteria imposed by ISO 148-2 [1].

Characterisation of the SB was carried out at IRMM using a pendulum verified according to the criteria imposed by ISO 148-2 [1]. The tests performed were within the scope of an ISO/IEC 17025 accreditation (BELAC 268-TEST).

Data evaluation was performed at IRMM. The certification project performed was within the scope of an ISO Guide 34 accreditation (BELAC 268-RM).

## 3 Processing

The ERM-FA415z test pieces were prepared from ASTM 565 XM-32 steel. The steel was cast and rolled into bars at Aubert&Duval (see Section 3.1). Production of the test pieces from these bars was performed at IfEP (see Sections 3.2, 3.4, 3.5 and 3.6). During each step of the processing care was taken to randomise the sequence of the test pieces.

### 3.1 Processing of hot-rolled bars

The base material consisted of ASTM 565 XM-32 steel produced at Aubert&Duval. To limit the amount of impurities potentially affecting the homogeneity of the fracture resistance, the following compositional tolerances specified in Table 1 were imposed on the selected steel batch. These tolerances are stricter than generally allowed for ASTM 565 steel.

Table 1: Adapted composition tolerances of ASTM 565 Grade XM-32

Composition (mass fraction, in g/kg)						
C	S	P	Si	Mn	Cr	Ni
1.1 – 1.3	< 0.03	<0.18	1.5 – 3	7.5 – 9	112.5 – 116.5	25.5 – 27.5
Mo	Cu	Al	V	W	N	
15.5 – 17	< 2	< 0.1	2.5 – 3	< 1	0.25 - 0.4	

The ingot was hot rolled, resulting in bars that were 6 m long and with a squared cross-section of 12 mm x 12 mm. For the ERM®- FA415z batch, steel was used from ingot number HM156901.

### 3.2 Machining of Charpy test pieces

9 bars numbered C1-C9 were cut into 941 Charpy specimens but not yet machined to the dimensional requirements of ISO 148-3 [9] by IfEP. Each specimen was engraved to ensure identification and traceability.

### 3.3 Heat treatment of hot-rolled bars

The heat treatment of the specimens was performed at VTN Witten GmbH (DE) in a vacuum-furnace. Two test heat treatments were done on a limited number of specimens (20 and 10 specimens respectively) to determine the conditions for the final heat treatment:

Step 1: austenisation treatment at 1040 °C for 30 minutes

Step 2: quenching with nitrogen (8 bars)

Step 3: first tempering at 695 °C for 120 minutes

Step 4: cool down with nitrogen (8 bars)

Step 5: second tempering at 660 °C for 120 minutes

Step 6: cool down with nitrogen (8 bars).

The specimens were distributed over 3 baskets. The baskets were stacked in the furnace and each basket had three thermocouples to monitor the temperature homogeneity. The measured temperatures at all positions were within the tolerance of  $\pm 6$  °C as required by IfEP.

### 3.4 Final machining of Charpy test pieces

After heat treatment, the specimens were machined to the final dimensions specified in ISO 148-3 [9] by IfEP. During this process the specimen numbers were transferred to one of the end faces. Finally the specimens were notched using a milling process.

### 3.5 Quality control

When all samples from the batch were fully machined, a random selection of 25 samples was made. The dimensions of the 25 samples were checked on against the dimensional criteria specified in ISO 148-3 [9] (length

55.0<sup>+0.00</sup><sub>-0.30</sub> mm, height 10.00 ± 0.06 mm, width 10.00 ± 0.07 mm, notch angle 45 ± 1°, height remaining at notch root 8.00 ± 0.06 mm, radius at notch root 0.250 ± 0.025 mm, distance between the plane of symmetry of the notch and the longitudinal axis of the test piece 27.5 ± 0.2 mm). All samples were within the ranges specified in ISO 148-3 [9].

The 25 samples checked for geometrical compliance were impact tested using a pendulum type MFL PSW 300 (nominal energy 300 J), verified in February 2012 according to ISO 148-2 [1].

The tests were done on November 27, 2012. The results are reported in the production report of November 28, 2012 [10]. The average *KV* of the 25 samples was 155.7 J, which is within the desired energy range (142.5 J to 157.5 J). The standard deviation of the test results (*s* = 3.0 J, *RSD* = 2.0 %) was below the 3.8 % maximum allowed by the contract. The variation was checked again during the characterisation tests at IRMM (see Section 6).

### 3.6 Packaging and storage

Finally, the samples were cleaned and packed in sets of 5 randomised samples, in oil-filled and vacuum sealed plastic bags. These oil-filled bags were packed in a sealed plastic bag carrying the label and shipped to IRMM. After arrival (December 5, 2012) the 885 samples (or 177 sets) of ERM-FA415z were registered and stored at room temperature (18 ± 5) °C, pending distribution.

## 4 Homogeneity

The test pieces are sampled from the SB, which is sufficiently, but not perfectly, homogeneous. Therefore, an appropriate homogeneity contribution  $u_h$  to the uncertainty of the certified value is required.  $u_h$  is related to  $s_h$ , the standard deviation between the samples in the SB (*sample-to-sample heterogeneity*), but also depends on the number of samples over which the *KV*-value is averaged. ISO 148-2 [1] specifies that the pendulum verification must be performed using 5 test pieces, which is why a CRM-unit consists of a set of 5 test pieces. The appropriate uncertainty contribution must be an estimate of the *set-to-set heterogeneity*, which in the case of a set of 5 test

pieces can be calculated as  $u_h = \frac{s_h}{\sqrt{5}}$ .

Here,  $u_h$  is estimated from  $s_h$ , the standard deviation of results obtained at IfEP on November 27, 2012 ( $s_h = 3.0$  J). This leads to  $u_h = 1.3$  J or 0.87 %.

As is required for a homogeneity test, the samples were randomly selected from the whole batch. The number of samples tested (25) is sufficiently large to reflect the homogeneity of the full SB (885 samples). It can be noted that  $u_h$  is probably a slight overestimation, since it contains also the repeatability of the instrument. However, the latter cannot be separated or separately measured.

## 5 Stability

The stability of the absorbed energy of Charpy V-notch certified reference test pieces was first systematically investigated for samples of nominally 120 J by Pauwels et al., who did not observe measurable changes of absorbed energy [11]. Additional evidence for the stability of the reference test pieces produced from AISI 4340 steel of lower energy levels (nominally 15 J, 30 J and 100 J) has been obtained during the International Master Batch (IMB) project [12]. In the IMB-project, the stability of the certified test pieces was judged from the change of the mean of means of the absorbed energy obtained on 7 reference pendulums over a three year period. None of the three regression slopes for the tested energy levels was statistically significant at the 0.05 significance level. Given the large sample-to-sample heterogeneity and the limited number of samples (5) in a CRM unit, the uncertainty contribution from instability is considered to be insignificant in comparison to that of homogeneity.

The main reason for the microstructural stability of the certified reference test pieces is the annealing treatment to which the samples were subjected after the austenisation treatment. Annealing is performed at temperatures where the equilibrium phases are the same as the (meta-)stable phases at ambient temperature ( $\alpha$ -Fe and  $\text{Fe}_3\text{C}$ ). The only driving force for instability stems from the difference in solubility of interstitial elements in the  $\alpha$ -Fe matrix, between annealing and ambient temperature. Relaxation of residual (micro-)stress by short-range diffusion or the additional formation or growth of precipitates during the shelf-life of the certified reference test pieces is expected to proceed but slowly.

In the meanwhile efforts are spent to better establish the stability of the certified values of batches of Charpy CRMs. Until such further notice, it is decided to specify a limited shelf-life. A period of 10 years is chosen, counting from the date of the characterisation tests on the SB. Since batch ERM-FA415z was characterised in January, 2013, the validity of the certificate expires in January, 2023.

## 6 Characterisation

### 6.1 Characterisation tests

30 samples from the SB ERM-FA415z (sets 1, 2, 3, 4, 5 and 6) were tested under conditions of repeatability with 25 samples from MB ERM-FA415s (sets 2, 3, 7, 10 and 11). The measurements were done using the Instron Wolpert PW 30 machine of IRMM, a Charpy impact pendulum yearly verified according to procedures described in ISO 148-2 [1]. Characterisation tests were performed on January 16, 2013 (laboratory temperature  $20 \pm 1$  °C), in accordance with ISO 148-1 [2]. The measurement sequence was: SB-MB-SB-MB-SB-MB-SB-MB-SB-MB-SB. The measured absorbed energy values were corrected for friction and windage losses.



The accepted data obtained on individual test pieces are shown in Figure 3 and Annex 1. The results of the measurements are summarised in Table 2.

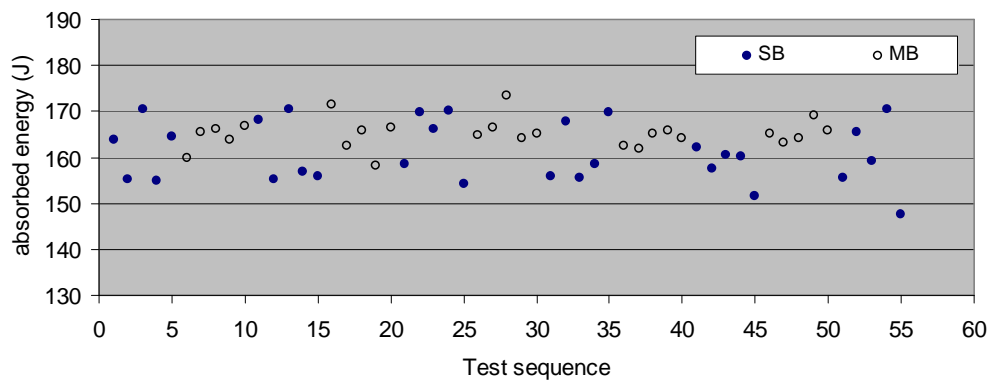


Figure 3: Absorbed energy values of 25 test pieces of ERM-FA415s compared with 30 test pieces of ERM-FA415z; data are displayed in the actual test sequence.

Table 2: Characterisation measurements of Batch ERM-FA415z

	Number of test pieces	Mean value	Standard deviation	Relative standard deviation
	$n_{MB}, n_{SB}$	$\bar{X}_{MB}, \bar{X}_{SB}$ [J]	$s_{MB}, s_{SB}$ [J]	$RSD_{SB}, RSD_{MB}$ [%]
<b>ERM®-FA415s (MB)</b>	25	165.07	3.17	1.92
<b>ERM®-FA415z (SB)</b>	30	161.05	6.56	4.07

The SB-results meet the ISO 148-3 acceptance criteria for a batch of reference materials ( $s_{SB} < 5\%$  for  $KV_{SB} > 40$  J).

## 6.2 Data from Master Batch ERM-FA415s

To calculate  $KV_{CRM}$  for ERM-FA415z one needs  $KV_{MB}$  of the MB used, i.e. ERM-FA415s. Table 3 shows the main MB-data, taken from the Certificate of Analysis of ERM-FA415s (Annex 2).

Table 3: Data from the certification of Master Batch ERM-FA415s

	Certified absorbed energy of Master Batch $KV_{MB}$ (J)	Standard uncertainty of $KV_{MB}$ $u_{MB}$ (J)	Relative standard uncertainty of $KV_{MB}$ $u_{MB,rel}$ (%)
<b>ERM®-FA415s</b>	157.3	1.4	0.89

### 6.3 Calculation of $KV_{CRM}$ and of $u_{char}$

From the data in Tables 2 and 3, and using Eq. 1,  $KV_{CRM}$  can be calculated:  $KV_{CRM} = 153$  J. Rounding of the certified value is done in accordance with the rounding of the associated uncertainty value (see Table . The uncertainty associated with the characterisation of the SB,  $u_{char}$ , is assessed as in Eq. 2 [8], which sums the relative uncertainties of the three factors in Eq. 1:

$$u_{char} = KV_{CRM} \sqrt{\frac{u_{MB}^2}{KV_{MB}^2} + \frac{s_{SB}^2}{n_{SB} \cdot \bar{X}_{SB}^2} + \frac{s_{MB}^2}{n_{MB} \cdot \bar{X}_{MB}^2}} \quad \text{Eq. 2}$$

$\bar{X}_{SB}$  and  $\bar{X}_{MB}$  were obtained under repeatability conditions. Therefore, the uncertainty of the ratio  $\bar{X}_{SB} / \bar{X}_{MB}$  is not affected by the contributions from reproducibility and bias of the pendulum used to compare MB and SB. Table 4 summarises the input quantities of the  $u_{char}$  uncertainty budget, their respective statistical properties, and shows how they were combined.

The effective number of degrees of freedom ( $\nu_{eff}$ ) for  $u_{char}$  is obtained using the Welch-Satterthwaite equation from the combined uncertainty ( $u_c$ ) and the individual uncertainty contributions ( $u_i$ ) and their respective degrees of freedom ( $\nu_i$ ) (Eq. 3) [6].

$$\nu_{eff} = \frac{u_c^4}{\sum_{i=1}^N \frac{u_i^4}{\nu_i}} \quad \text{Eq. 3}$$

Table 4: Uncertainty budget for the characterisation tests of ERM-FA415z

FA415z	source of uncertainty	measured value (J)	standard uncertainty (J)	probability distribution	divisor	sensitivity coefficient	relative uncertainty (%)	degrees of freedom
$KV_{MB}$	Certification of MB	157.3	1.4	normal	1	1	0.89	6
$\bar{X}_{SB}$	comparison of SB and MB in repeatability conditions	161.05	1.20	unimodal	1	1	0.74	29
$\bar{X}_{MB}$		165.07	0.63	normal	1	1	0.38	24
$u_{char,rel} \text{ (}\% \text{)}$							1.22	19
$u_{char} \text{ (J)}$							1.87	

## 7 Value assignment

### 7.1 Certified value, combined and expanded uncertainty

As shown in 6.3,  $KV_{CRM} = 153$  J. The uncertainty of the certified value is obtained by combining the contributions from the characterisation study,  $u_{char}$ , and from the homogeneity assessment,  $u_h$ , as is summarized in the following uncertainty budget (Table 5).

The relevant number of degrees of freedom calculated using the Welch-Satterthwaite equation [6], is sufficiently large ( $\nu_{RM} = 35$ ) to justify the use of a coverage factor  $k = 2$  to expand the confidence level to about 95 %. The obtained expanded uncertainty provides justification for the SB-MB approach followed:  $U_{CRM}$  is sufficiently smaller ( $U_{CRM} = 3.0$  %) than the verification criterion of 10 % for industrial pendulums [1] or even 5 % for reference pendulums [9].

Table 5: Uncertainty budget for the certified value  $KV_{CRM}$  of ERM-FA415z

	source of uncertainty	relative value $u_i$ (%)	degrees of freedom
$u_{char}$	characterisation of SB	1.22	19
$u_h$	homogeneity of SB	0.87	24
Combined standard uncertainty, $u_{CRM}$ (%)		1.50	35
Combined standard uncertainty, $u_{CRM}$ (J)		2.30	
Expanded Uncertainty, $k = 2$ , $U_{CRM}$ (%)		3.00	
Expanded Uncertainty, $k = 2$ , $U_{CRM}$ (J)		5	

## 8 Metrological traceability and commutability

The certified property is defined by the Charpy pendulum impact test procedure described in ISO 148-1 [2].

The certified value of the MB ERM-FA415s is traceable to the SI, since it was obtained using an interlaboratory comparison, involving a representative selection of qualified laboratories performing the tests in accordance with the standard procedures and using instruments verified and calibrated with SI-traceable calibration tools.

The certified value of ERM-FA415z is made traceable to the SI-traceable certified value of the MB by testing SB and MB samples in repeatability conditions on an impact pendulum verified and calibrated with SI-traceably calibrated tools. Therefore, the certified value of ERM-FA415z is traceable to the International System of Units (SI) via the corresponding Master Batch ERM-FA415s of the same nominal absorbed energy (150 J). Absorbed energy  $KV$  is a method-specific value, and can only be obtained by following the procedures specified in ISO 148-1 [2].

The intended use of the certified reference test pieces is the verification of Charpy impact pendulums. The material chosen to produce the CRM is an industrial type of steel, representative for the materials typically tested with Charpy impact pendulums. Therefore, the samples have an interaction with the pendulum that is comparable to routine samples, thus ensuring commutability of the CRM. However, during the certification of the SB and the

MB different pendulums were used, each equipped with an ISO-type striker of 2 mm tip radius. Until further notice, the certified values are not to be used when the test pieces are broken with an ASTM-type striker of 8 mm tip radius [11].

## **9 Instructions for use**

### **9.1 Safety information**

Precautions need to be taken to avoid injury of the operator by broken specimens when operating the Charpy impact pendulum.

### **9.2 Intended use**

Samples of ERM-FA415z correspond to the 'certified reference test pieces' as defined in ISO 148-3 [9]. Sets of five of these certified reference test pieces are intended for the indirect verification of impact testing machines with a striker of 2 mm tip radius according to procedures described in detail in ISO 148-2 [1].

The indirect verification provides an assessment of the bias of the user's Charpy pendulum impact machine. This bias assessment can be used in the calculation of the measurement uncertainty of Charpy tests on the pendulum after indirect verification. Such uncertainty calculation requires the certified value, the associated uncertainty, and in some cases also the degrees of freedom of the uncertainty, all given on page 1 of the certificate.

### **9.3 Sample preparation**

Special attention is drawn to the cleaning of the specimens prior to the tests. It is mandatory to remove the oil from the sample surface prior to testing, without damaging the edges of the sample. Between the moment of removing the protective oil layer and the actual test, corrosion can occur. This must be avoided by limiting this period of time, while keeping the sample clean.

The following procedure is considered a good practice.

1. First use absorbent cleaning-tissue to remove the excess oil. Pay particular attention to the notch of the sample, but do not use hard (e.g. steel) brushes to remove the oil from the notch.
2. Submerge the samples in ethanol for about 5 min. Use of ultrasonication is encouraged, but only if the edges of the samples are prevented from rubbing against each other. To reduce the consumption of solvent, it is allowed to make a first cleaning step with detergent, immediately prior to the solvent step.
3. Once samples are removed from the solvent, only manipulate the samples wearing clean gloves. This is to prevent development of corrosion between the time of cleaning and the actual test.
4. Before testing, bring the specimens to the test temperature ( $20 \pm 2$ ) °C. To assure thermal equilibrium is reached, move the specimens to the test laboratory at least 3 h before the tests.

#### **9.4 Pendulum impact tests**

After cleaning, the 5 samples constituting a CRM-unit need to be broken with a pendulum impact test machine in accordance with ISO 148-1 [2]. Prior to the tests, the anvils must be cleaned. It must be noted that Charpy test pieces sometimes leave debris on the Charpy pendulum anvils. Therefore, the anvils must be checked regularly and if debris is found, it must be removed. The uncertainty of the certified value applies to the mean of the five *KV*-values.

#### **9.5 Storage**

Specimens should be kept at room temperature ( $18 \pm 5$ ) °C in their original packing until used. The European Commission cannot be held responsible for changes that happen during storage of the material at the customer's premises, especially of opened samples.

### **Acknowledgements**

The authors wish to thank V. Kestens, A. Held, R. Koeber, and H. Emons (all IRMM) for reviewing the certification report.

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## Annex 1

Results of characterisation measurements of ERM-FA415z as measured according to ISO 148-1 at IRMM, January 16, 2013.

	Master Batch ERM-FA415s	Secondary Batch ERM-FA415z
	<i>KV (J)</i>	<i>KV (J)</i>
1	159.93	163.89
2	165.40	155.15
3	166.03	170.58
4	163.69	155.02
5	166.69	164.42
6	171.47	168.05
7	162.59	155.15
8	165.71	170.46
9	158.16	156.79
10	166.37	156.01
11	164.81	158.36
12	166.57	169.87
13	173.36	166.18
14	164.23	170.07
15	165.01	154.24
16	162.35	156.01
17	161.96	167.74
18	165.28	155.42
19	165.67	158.43
20	164.11	169.68
21	165.08	162.15
22	163.13	157.45
23	164.30	160.39
24	169.17	160.19
25	165.67	151.56
26		155.69
27		165.47
28		159.22
29		170.33
30		147.43
<b>Mean (J)</b>	<b>165.07</b>	<b>161.05</b>
<b>Standard deviation (J)</b>	<b>3.17</b>	<b>6.56</b>
<b>RSD (%)</b>	<b>1.92</b>	<b>4.07</b>

## Annex 2



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# CERTIFICATE OF ANALYSIS

ERM<sup>®</sup> - FA415s

STEEL CHARPY V-NOTCH TEST PIECES		
	Impact toughness	
	Certified value <sup>2)</sup> [J]	Uncertainty <sup>3)</sup> [J]
Absorbed energy (KV) <sup>1)</sup>	157.3	1.4
<p>1) The absorbed energy (KV) is procedurally defined and refers to the impact energy required to break a V-notched bar of standardised dimensions, as defined in ISO 148-1. The certified value is only valid for strikers with a 2 mm tip radius and in the temperature range of (20 ± 2) °C.</p> <p>2) The certified value is estimated as the mean of means of absorbed energies measured on 7 pendulums in 5 different laboratories. On each pendulum, 20 test pieces were broken. The pendulums used are regularly verified with equipment that is calibrated in a manner that is traceable to the International System of Units (SI). Therefore, the certified value is traceable to the International System of Units (SI).</p> <p>3) Standard uncertainty <math>u</math> of the certified mean absorbed energy of batch ERM-FA415s, estimated as the standard error of the mean of the 7 pendulum mean values, corresponding with a confidence level of about 68 %, as defined in the ISO/IEC Guide 98-3:2008; Uncertainty of measurement – Part 3: Guide to the expression of uncertainty in measurement (GUM). The number of degrees of freedom of the certified uncertainty, <math>\nu_{RM} = 6</math>.</p>		

This certificate is valid until December 2021.

### NOTE

European Reference Material ERM<sup>®</sup>-FA415s was produced and certified under the responsibility of the Institute for Reference Materials and Measurements of the European Commission's Joint Research Centre according to the principles laid down in the technical guidelines of the European Reference Materials<sup>®</sup> co-operation agreement between BAM-IRMM-LGC. Information on these guidelines is available on the internet (<http://www.erm-crm.org>).

Accepted as an ERM<sup>®</sup>, Geel, July 2012  
Latest revision: September 2012

Signed: \_\_\_\_\_

Prof. Dr. Hendrik Emons  
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Joint Research Centre  
Institute for Reference Materials and Measurements  
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Registration No. 268-RM  
ISO Guide 34 for the  
production of reference materials

All following pages are an integral part of the certificate.

Page 1 of 3



## DESCRIPTION OF A CRM UNIT

A unit consists of five Charpy V-notch test pieces, which are rectangular steel bars of nominal dimensions 55 mm x 10 mm x 10 mm, with one V-notch, accurately machined to tolerances imposed in ISO 148-3. The five specimens are packed together in a plastic bag filled with oil to prevent oxidation.

## METHOD USED FOR CERTIFICATION

Charpy pendulum impact tests in accordance with ISO 148-1, using pendulum impact machines with a 2 mm striker tip radius.

## PARTICIPANTS

### Processing

- Cogne Acciai Speciali, Aosta, IT: production of steel bars
- Aubert & Duval, Gennevilliers, FR: heat treatment of steel bars
- Laboratoire National de Métrologie et d'Essais (LNE), Trappes, FR: processing of the V-notch test pieces

### Characterisation

- Exova, Emmen, NL (RvA testen L085)\*
- Bundesanstalt für Materialforschung und -prüfung (BAM), Division 9.1 Random Loading Fatigue and Structural Integrity, Berlin, DE (DGA-PL-2614.16)\*
- Centro de Apoio Tecnológico a Indústria Metalomecânica (CATIM), Laboratório de Ensaios, Porto, PT (IPAC L009)\*
- Fraunhofer Gesellschaft, Institut für Werkstoffmechanik, Freiburg, DE
- European Commission Joint Research Centre (JRC), Institute for Reference Materials and Measurements, Geel, BE (BELAC 268-Test)\*
- Laboratoire National de Métrologie et d'Essais, Charpy Laboratory, Trappes, FR (COFRAC SMH 2-1287)\*
- National Institute of Standards and Technology (NIST), Materials Reliability Division, Boulder, USA
- SCK-CEN, Labo Reactormaterialenonderzoek, Mol, BE (BELAC 015-Test)\*
- SIRRIS, Beproevinglaboratorium Gent, Zwijnaarde, BE (BELAC 232-Test)\*
- Universität Stuttgart, Materialprüfungsanstalt, Stuttgart, DE (DAP-PL-2907.02)\*

\* Measurements within the scope of accreditation to ISO/IEC 17025.

## SAFETY INFORMATION

Precautions need to be taken to avoid injury of the operator by broken specimens when operating the Charpy impact pendulum.

## INTENDED USE

Test pieces of ERM-FA415s correspond with the 'certified' BCR test pieces' as referred to in (the now obsolete) EN 10045-2 (Method for the verification of impact testing machines), as well as with the 'certified reference test pieces' as defined in ISO 148-3 (Preparation and characterisation of Charpy V reference test pieces for verification of test machines).

The ERM-FA415s batch is one of the 'Master Batches'. Master Batch test pieces are not for sale. They are intended solely to traceably certify Secondary Batches of the same nominal absorbed energy (here 150 J). The certified value of the Master Batch, and its associated uncertainty, are used in the calculation of the certified value and combined and expanded uncertainty of a unit of 5 specimens from a Secondary Batch. Because the certified value of the Master Batch, and its uncertainty, are intermediate values, the standard uncertainty was not expanded to the 95 % confidence level, thereby avoiding unnecessary rounding effects.

When characterising a secondary batch, a number of Master Batch test pieces are broken under repeatability conditions together with a selection of test pieces from the secondary batch.

## INSTRUCTIONS FOR USE

Special attention is drawn to the cleaning and conditioning of the specimens prior to testing. It is mandatory to remove the oil from the test piece surface prior to testing, without damaging the edges of the test piece. Between the moment of removing the protective oil layer and the actual test, corrosion can occur. This must be avoided by limiting this period of time, while keeping the test piece clean.

The following cleaning and conditioning procedure is considered to be good practice.

1. First use absorbent cleaning-tissue to remove the excess oil. Pay particular attention to the notch of the test piece, but do not use hard (e.g. steel) brushes to remove the oil from the notch.
2. Submerge the test pieces in technically pure ethanol for about 5 minutes. Use of ultrasonication is encouraged, but only if the edges of the test pieces are prevented from rubbing against each other. To reduce the consumption of solvent, it is allowed to make a first cleaning step with detergent, immediately prior to the solvent step.
3. Once test pieces are removed from the solvent, only manipulate the test pieces wearing clean gloves. This is to prevent development of corrosion between the time of cleaning and the actual test.
4. Before testing, bring the specimens to the test temperature ( $20 \pm 2$  °C). To assure thermal equilibrium is reached, move the specimens to the test laboratory at least 3 h before the tests.

After cleaning and equilibration, the test pieces need to be broken with a pendulum impact test machine operated in accordance with ISO 148-1, including the correction of the raw data for friction. Prior to the tests, the anvils must be cleaned. It must be noted that Charpy test pieces sometimes leave debris on the Charpy pendulum anvils. Therefore, the anvils must be checked regularly and if debris is found, it must be removed.

## STORAGE

Specimens should be kept at room temperature ( $18 \pm 5$  °C) in their original packing until used. The European Commission cannot be held responsible for changes that happen during storage of the material at the customer's premises, especially of opened units.

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## NOTE

A detailed technical report is available on [www.irmm.jrc.be](http://www.irmm.jrc.be). A paper copy can be obtained from the Joint Research Centre, Institute for Reference Materials and Measurements on request.

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European Commission

**EUR 25798 EN – Joint Research Centre – Institute for Reference Materials and Measurements**

Title: The certification of the absorbed energy (150 J nominal) of Charpy V-notch reference test pieces for tests at 20 °C: ERM®-FA415z

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**Abstract**

This certification report describes the processing and characterisation of ERM®-FA415z, a batch of Charpy V-notch reference test pieces certified for the absorbed energy (KV) for tests at 20 °C. Sets of five of these test pieces are used for the verification of pendulum impact test machines according to ISO 148-2 (Metallic materials - Charpy pendulum impact test – Part 2: Verification of testing machines [1]).

The measurand KV is procedurally defined and refers to the impact energy required to break a V-notch test piece of standardised dimensions, as defined in ISO 148-1 [2]. The certified value of ERM- FA415z is traceable to the SI, via the SI-traceable certified value of the master batch ERM-FA415s, by testing samples of ERM-FA415z and ERM-FA415s under repeatability conditions on an impact pendulum verified and calibrated with SI-traceably calibrated tools. The certified value is valid only for strikers with a 2 mm tip radius. The certified values are valid at  $(20 \pm 2)$  °C.

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